

Chapter 10. Chain-Growth Polymerization()

10.1. Introduction

Step - Growth

-
- 가
-
- high conversion high MW
long reaction time

Chain - Growth

-
- radical anionic, cationic, reaction site
monomer unit
size .
- active species active center
- kinetic chain reaction
.

Free Radical	Free Radical Initiation
Cationic } Ionic	Cationic Initiation
Anionic	Anionic Initiation

Kinetic Chain Reaction()

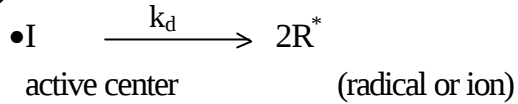
-
- 가
 - 1) (Initiation)-
 - 2) (propagation)-
 - 3) (termination)-kinetic chain
(chain transfer)-physical chain
kinetic chain

Kinetic Chain Length() : v

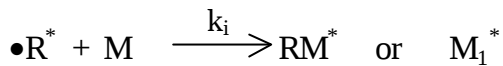
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10.2. General Kinetic Scheme

1) Initiation



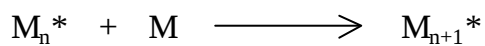
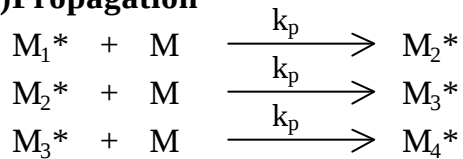
$$k_d: \quad \sim 10^{-4} \sim 10^{-6} \text{ l/mole} \cdot \text{sec}$$



↑
(primary active species or primary radical or
initiator radical)

$$k_i:$$

2) Propagation

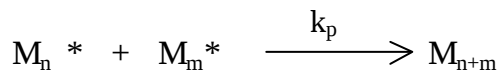


$$k_p: \quad 10^2 \sim 10^4 \text{ l/mole} \cdot \text{sec} \quad \text{step-growth}$$

3) Termination

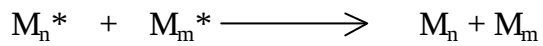
- (coupling or combination): Kinetic chain length 가
polymer 가

$$\overline{DP}_n = 2 \nu$$

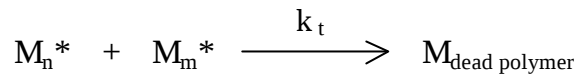


- (不均化, disproportionation)
: kinetic chain length 가 polymer 가
 $\overline{DP}_n = \nu$

$$k_{td}$$



•



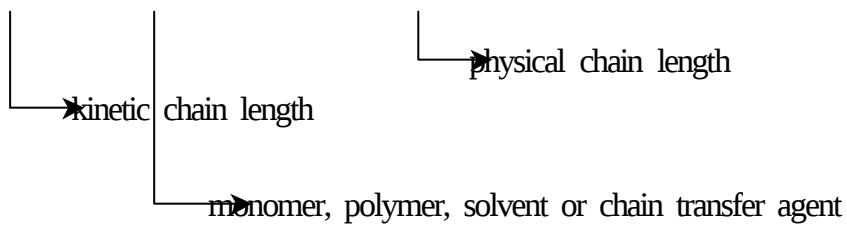
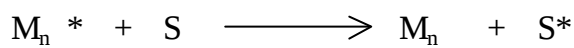
$$k_t = k_{tc} + k_{td} \quad \sim 10^6 - 10^8 \text{ l/mole} \cdot \text{sec}$$

* k_p 가 k_t _____ ?

① radical species 가

② _____ 가 k_t 1/2

4) Chain Transfer



Kinetic Chain Length()

: (v)
ex) 4 가 4000 disproportionation

$$v = 4000 / 4 = 1000$$

step 1, 2, 3

, Chain Transfer 가

Physical Chain Length():

Step 1, 2, 3, 4

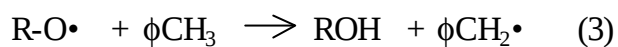
10.3. Kinetic Chain Reaction

10.3.1. Non-Polymerization Reaction

Peroxide induced bromination of toluene

1) Initiation

Two types of reaction

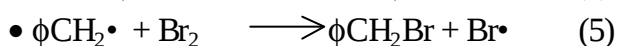


ROOR

가

kinetic chain

2) Propagation



benzyl bromide

(4)

 $\text{Br}\cdot$

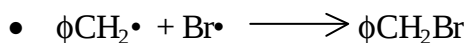
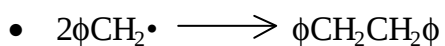
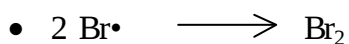
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가

active species

kinetic chain reaction

3) Termination



kinetic chain

•

NET EFFECT OF KINETIC Chain rexn:

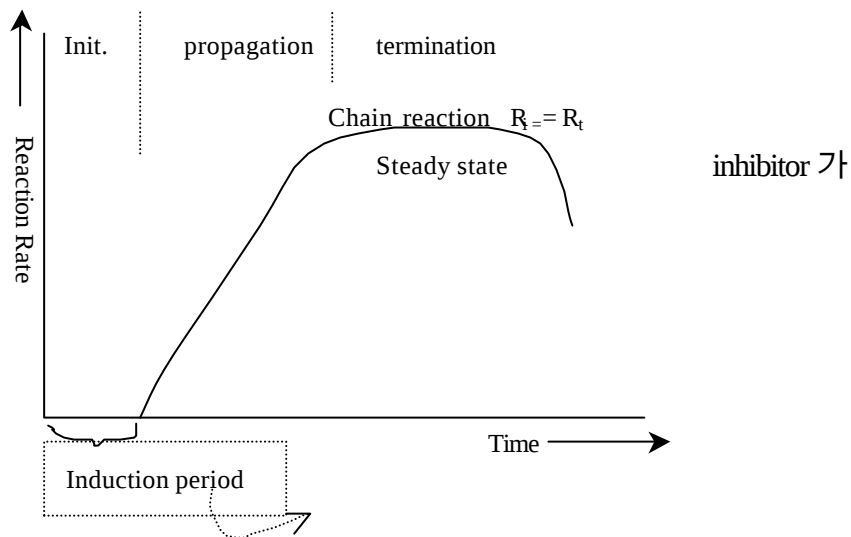
One ROOR molecule can cause the formation of Br_2 , $\phi\text{CH}_2\text{CH}_2\phi$, $\phi\text{CH}_2\text{Br}$,

 $\text{HBr},$

1

10.3.2. Non-Chain Chain Polymerization Reaction

non-chain chain polymerization reaction



Chain reaction (induction period) 가 .
 inhibitor 가 . active center 가
 가 (steady state)
 . 가 plateau region level
 off . , .

Linear Chain-Growth polymerization : polymer of high $\overline{DP}_n$ found easily in early reaction

Linear Step-Growth polymerization : high extent of reaction value required to obtain high $\overline{DP}_n$

10.3.3. Free Radical

Ionic Reaction

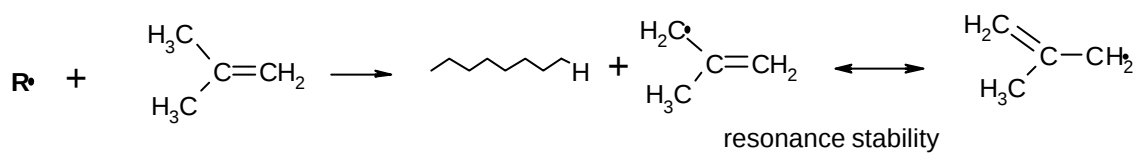
- Ionic Initiation – multiple bond addition ring opening polymerization
- Radical Initiation – ring-opening polymerization

Free Radical ionic , mechanism

Ex)



will not produce free radical

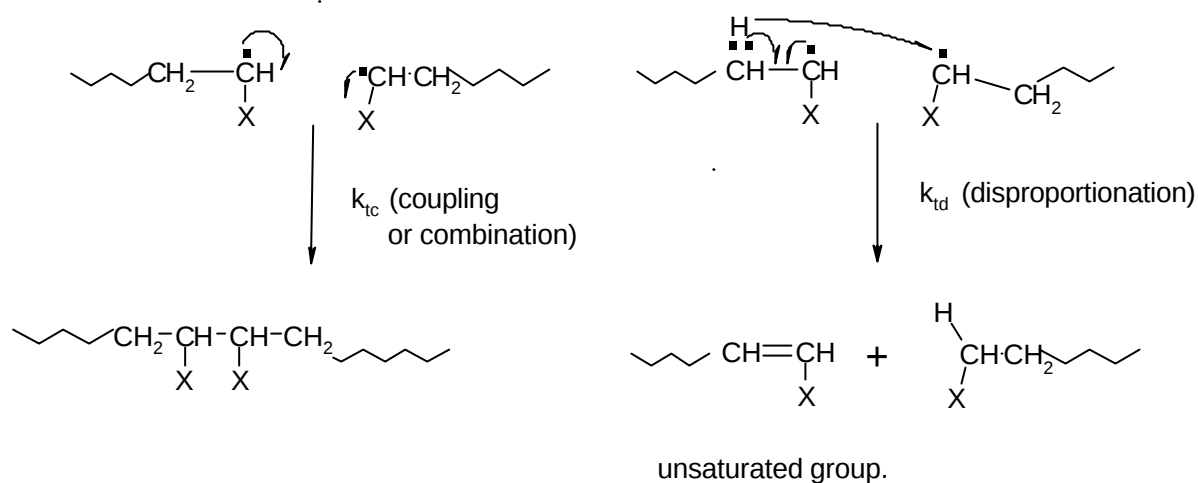


)

	Ionic		Free Radical
	Anionic	Cationic	
Ring opening	+	-	-
End-groups	counter-ion gegenion e.g. $R-\overset{+}{Al}Cl_4-\overset{-}{O}$ Degree of association Solvent-system polarity End group stability Type & size of scounter-ion Temp. Degree of association influenences: Reaction rates Termination rate Stereospecificity(stereoregular polymer)		Truly Free Radical (no association)
Termination Step	Living polymer Block copolymer 가	Radical (unimolecular combination) (disproportionation)	(bimolecular) combination disproportionation 가

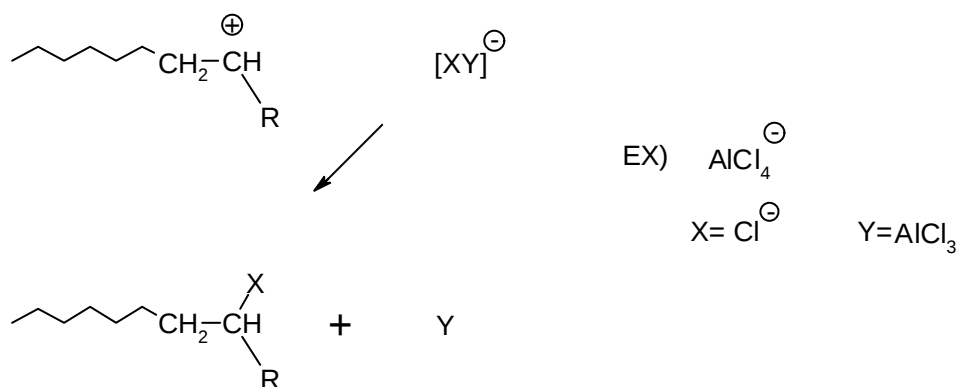
10.3.4. Free Radical Reaction Ionic Reaction Termination Step

A) Free Radical Termination

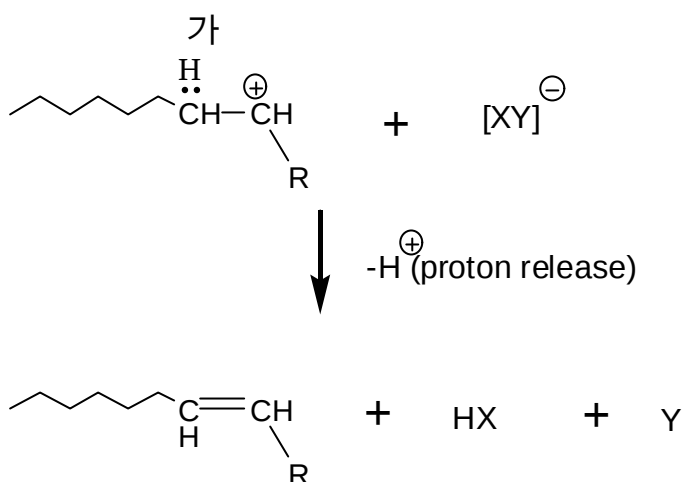


Two molecules involved
= **bimolecular reaction**

B) Cationic Termination



anionic capture free radical combination
MW 가 . (unimolecular reaction)

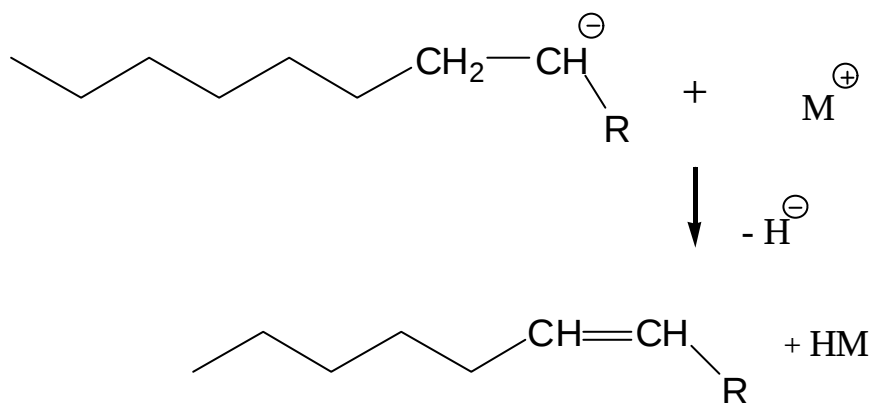


proton release free radical disproportionation

(unimolecular reaction)

C) Anionic Termination

Termination is rare but can occur by loss of a hydride ion(H^-)



Unimolecular type termination occurs

	Anionic Termination	Cationic Termination	Free Radical Termination
Reaction rate	Unimolecular Unimolecular High concentration of growing chains $10^{-2} \sim 10^{-3}$ molar Rates $10^4 \sim 10^5$ times higher than free radical		Bimolecular Relatively low concentration of growing chains $10^{-8} \sim 10^{-9}$ molar occurs at high rates
ΔE	Activation Energies Similar		
Chain Transfer	Negligible	+	+
Disadvantage	Rigorous Purity or precautions (free of water)		
Polymer System	Solution or Bulk		Wide variety of polymer systems, Gas, Solid, Solution, Bulk, Precipitation, Suspension, Emulsion

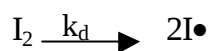
10.3.5 Free Radical Initiated Polymerization of Unsaturated monomers

Kinetic Scheme

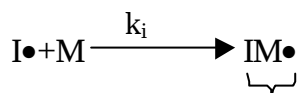
1) Initiation

Two step sequence-Both enter into overall rate

1. Initiator decomposition



2. Initiator fragment $I\bullet$ $\xrightarrow{k_i}$ $IM\bullet$, chain growth



$IM\bullet$
Primary radical species

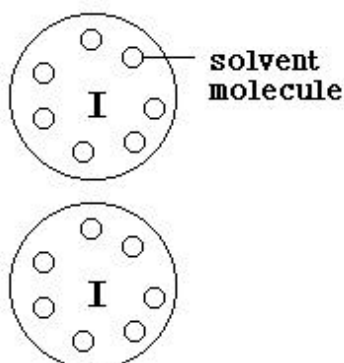
Initiator efficiency(f) = $\frac{\text{desired reaction}}{\text{desired reaction} + \text{side reaction}}$

.

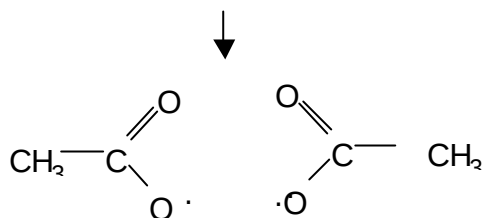
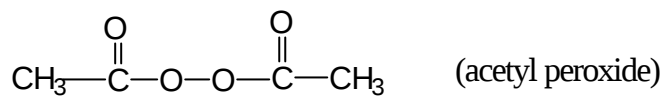
, $0.5 < f < 1$

a. Cage Effect – primary recombination

Initiator fragments surrounded by restricting cage of solvent

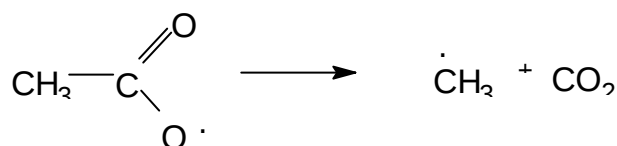


Ex)



i. Recombination possible $\text{I}_2 \rightleftharpoons 2\text{I}\cdot$

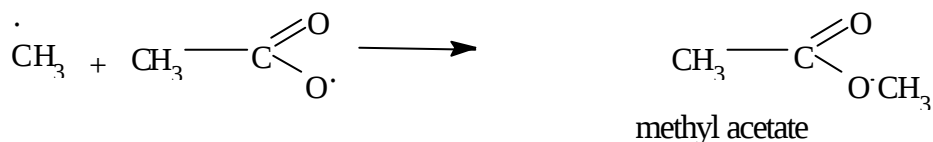
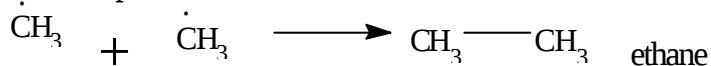
ii. free radical cage elimination reaction



Radical combination

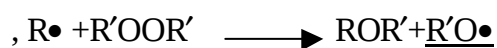
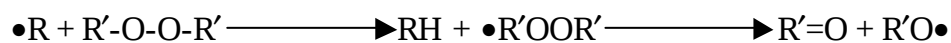
가 .

Inactive Species



b. Induced Decomposition – secondary combination

i. radical peroxide

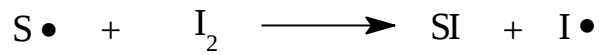
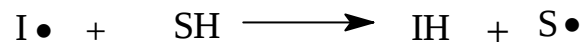


peroxide

total number of radical

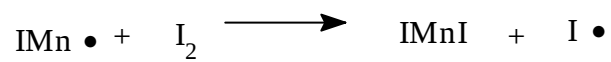
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ii. Chain Transfer to Solvent



.

iii. Reaction with Chain Radical



가

efficiency factor

.

f: Initiator Efficiency

=mole fraction of initiator fragments that actually initiate polymer chains.

$$0.5 < f < 1.0$$

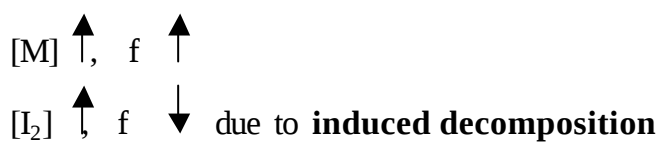
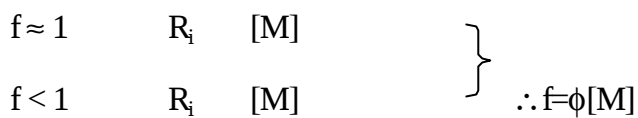
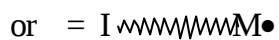
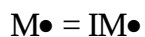
c. Reaction Rate

$$\begin{aligned} R_i &= \frac{d[M \bullet]}{dt} \\ &= k_i [I \bullet] [M] \\ &= 2 f k_d [I_2] \end{aligned}$$

by convention, radical
2 .

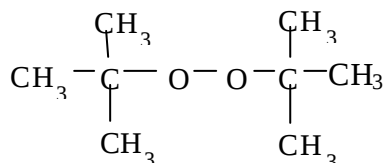
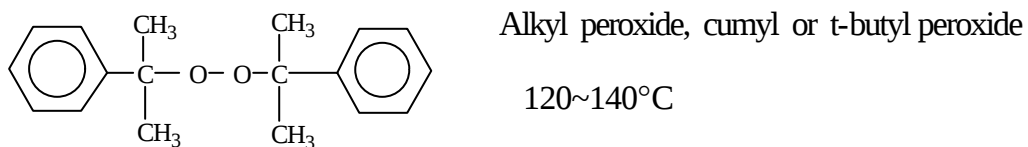
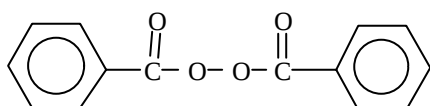
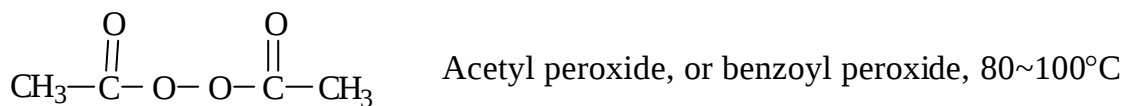
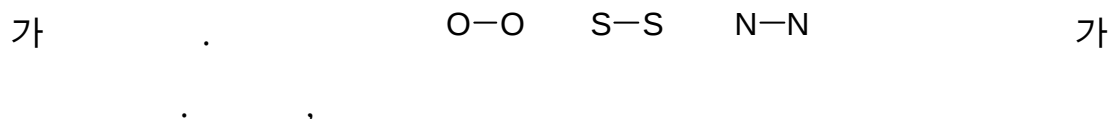
$[M \bullet]$ 가

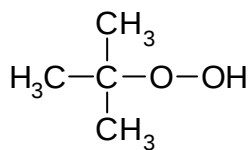
chain radical



d. Initiator

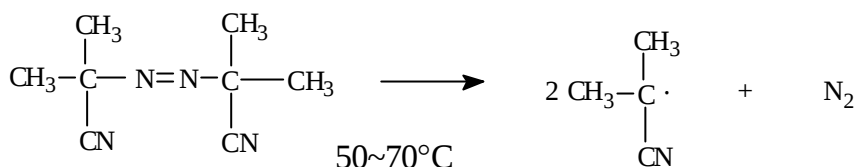
thermal decomposition





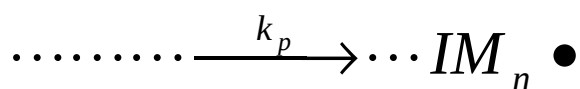
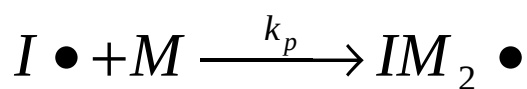
Hydroperoxides(cumyl or t-butyl)

80~100°C



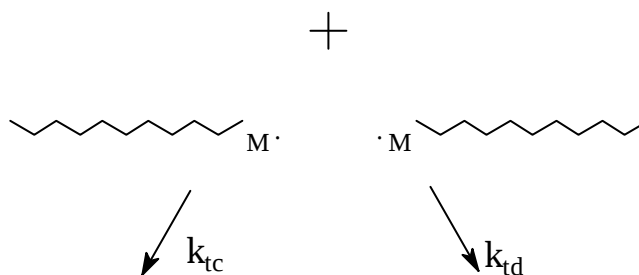
AIBN (2,2' azobisisobutyronitrile)

3) Propagation



$$R_p = -\frac{d[M]}{dt} = k_p [M][M\cdot]$$

3) Termination



$$R_t = -\frac{d[M\cdot]}{dt} = 2(k_{tc} + k_{td})[M\cdot]^2$$

By convention
2

4) Overall Rate of Polymerization.

$$R_o = k_i[I\bullet][M] + k_p[M\bullet][M]$$

(# of propagation step >>> # of initiation step) $\therefore$

$$R_o \sim R_p = k_p[M][M\bullet]$$

Radical concentration

- $[M\bullet]$ is very low ($\sim 10^{-8}$ molar).
- $[M\bullet]$ is a function of R_o .
- $[M\bullet]$ is a function of R_o .

$[M\bullet]$

Steady-State Assumption

At steady state, $[M\bullet]$ is constant.
 reaction rate change $\frac{d[M\bullet]}{dt} = 0$.
 (active centers created and destroyed at the same time)

$$R_i = R_t$$

$$2fk_d[I_2] = 2(k_{tc} + k_{td})[M\bullet]^2$$

$$\therefore [M\bullet] = \left(\frac{fk_d}{k_{tc} + k_{td}}\right)^{\frac{1}{2}} [I_2]^{\frac{1}{2}}$$

$$\text{or } [M\bullet] = \left[\frac{R_i}{2R_t}\right]^{\frac{1}{2}}$$

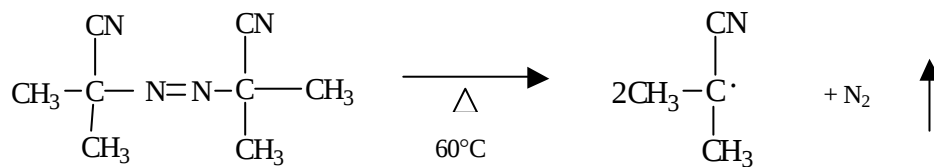
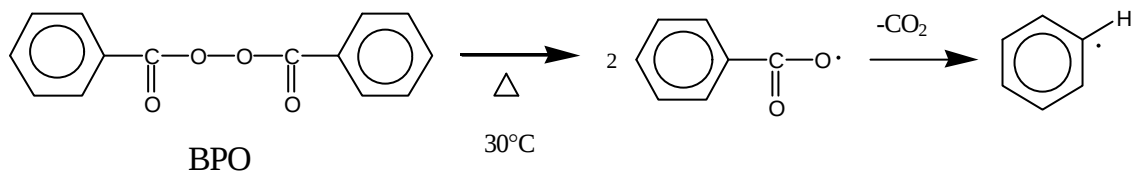
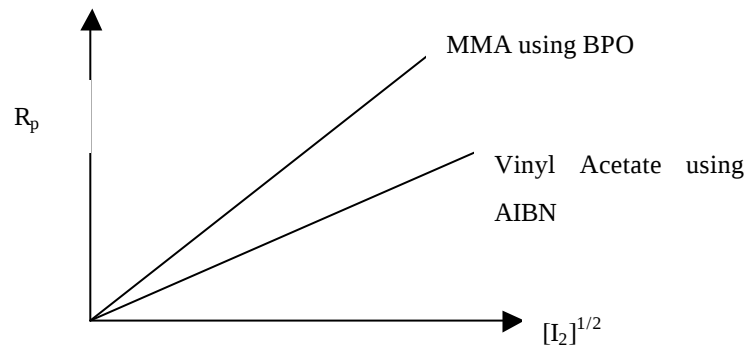
$1/2$

recall $R_p = -\frac{d[M]}{dt} = k_p[M][M\bullet]$

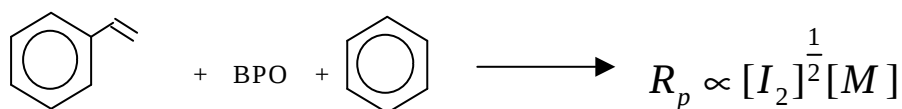
$R_p = k_p[M][I_2]^{\frac{1}{2}} \left(\frac{fk_d}{k_{tc} + k_{td}}\right)^{\frac{1}{2}}$

$f < 1$ system $[I_2]^{1/2}$ 가 . square root dependence of $[I_2]$.

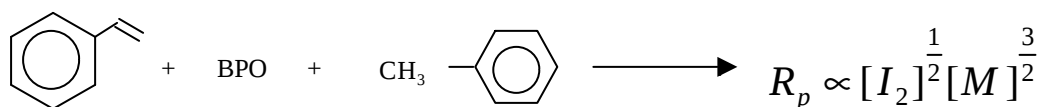
☛ Odian Fig. 3-4



Azobisisobutyronitrile



$f < 1$ SRD 가



f 가 $[M]$ dependent .

{ Why? }

Due to induced decomposition of toluene t[I₂]

10.4 Kinetic Chain Length (KLC)

At Steady-State assumption

1) Disproportionation

$$KCL = \frac{R_p}{R_t (= R_i)} \quad (\text{polymer chain})$$

Knowing that

$$R_t = R_{td} + R_{tc} = -\frac{d[M\bullet]}{dt}$$

2) Coupling or combination

$$R_{tc} = -\frac{d[M\bullet]}{dt} \Big|_{term} = \frac{1}{2} k_{tc} (M\bullet)^2 \quad (\because \text{2 } M\bullet \rightarrow 1 \text{ polymer chain})$$

3)

$$\begin{aligned} KCL &= \frac{R_p}{R_t} = \frac{R_p}{R_{td} + \frac{1}{2} R_{tc}} = \frac{2R_p}{R_{td} + \underbrace{R_{tc} + R_{td}}_{R_t}} \\ &= \frac{2R_p}{R_t \left(1 + \frac{R_{td}}{R_t}\right)} \end{aligned}$$

define $y = \frac{R_{td}}{R_t}$: fraction of termination caused by disproportionation

$$KCL = \frac{2R_p}{R_t(1+y)}$$

$\overline{DP}$ ① 가 가 ↑
 ② 가 ↑

$$\overline{DP}_n = \frac{-d[M]/dt}{d[Polymer]/dt} = \frac{-d[M]/dt}{d[Polymer]/dt}$$

1) Dispropotionation

$$\overline{DP}_n = n$$

2) Coupling

$$\overline{DP}_n = 2n$$

3)

$$\begin{aligned}
 \text{Polymer} &= R_{td} + \frac{1}{2} R_{tc} \\
 &= R_p
 \end{aligned}$$

$$\overline{DP}_n = \frac{R_p}{R_{td} + \frac{1}{2} R_{tc}} = \frac{2 R_p}{R_t (1 + y)} \dots (1) \quad \text{where} \quad y = \frac{R_{td}}{R_t}$$

$$\overline{DP}_n = \frac{2n}{1 + y}$$

$$\text{knowing that} \quad R_p = k_p \left\{ \frac{k_d}{k_t} f[I_2] \right\}^{\frac{1}{2}} [M] \dots (2)$$

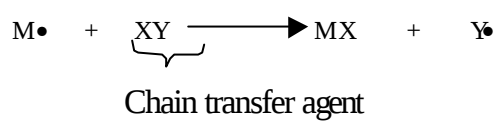
$$R_t = R_i = 2 f k_d [I_2] \dots (3)$$

(1),(2),(3) Chain transfer 가 steady-state assumption

$$\begin{aligned}
 \overline{DP}_n &= \frac{k_p [M]}{(1 + y) k_t \left\{ \frac{k_d}{k_t} f[I_2] \right\}^{\frac{1}{2}}} \dots (4) & ? \\
 & & (2),(4)
 \end{aligned}$$

$$\text{or } \overline{DP_n} = \frac{k_p^2 [M]^2}{(1+y)k_t R_p} \dots\dots(5)$$

10.5 Chain Transfer

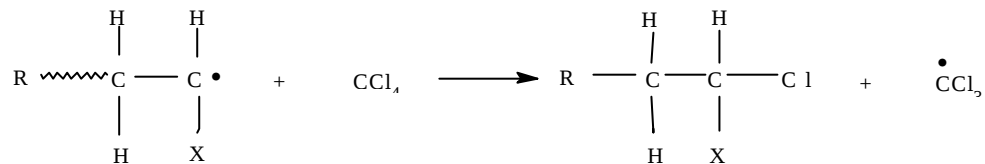


Chain transfer 가 R_p $\overline{DP_n}$

.

$$(R_p = k_p [M][M\bullet] \quad [Y\bullet])$$

ex)



(1) 가 chain transfer agent transfer 가 .

chain transfer coefficient 가 .

(2) transfer 가 .

Inhibitor and Retarder

● Inhibitor ()

$Y\bullet$.

hydroquinone

.

● Retarder ()

Y●

,

MW

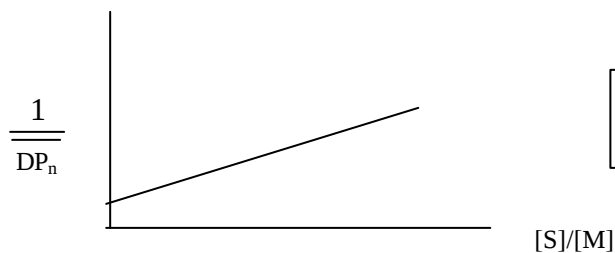
mercaptan

.

chain transfer 가

$$\begin{aligned} \frac{d[\text{Polymer}]}{dt} &= R_{td} + \frac{1}{2}R_{tc} + \sum R_{tr} \\ \therefore \overline{DP}_n &= \frac{R_p}{\frac{d[\text{Polymer}]}{dt}} = \frac{2R_p}{R_t(1+y) + 2\sum R_{tr}} \\ &= \frac{2k_p[M][M\bullet]}{2k_t[M\bullet]^2(1+y) + 2\sum k_{tr}[M\bullet][XY]} \\ &= \frac{k_p[M]}{k_t[M\bullet](1+y) + \sum k_{tr}[XY]} \\ \text{Knowing that } [M\bullet] &= \left\{ \frac{k_d f}{k_t} [I_2] \right\}^{\frac{1}{2}} \end{aligned}$$

$$\begin{aligned} \overline{DP}_n &= \frac{k_p[M]}{k_t(1+y) \left\{ \frac{k_d f}{k_t} [I_2] \right\}^{\frac{1}{2}} + \sum k_{tr}[XY]} \\ \frac{1}{\overline{DP}_n} &= \frac{k_t(1+y)}{k_p[M]} \left\{ \frac{k_d f}{k_t} [I_2] \right\}^{\frac{1}{2}} + \frac{\sum k_{tr}[XY]}{k_p[M]} \\ \frac{1}{\overline{DP}_n} &= \frac{1}{\overline{DP}_{n,0}} + \frac{k_{tr,s}[S]}{k_p[M]} + \frac{k_{tr,t}[T]}{k_p[M]} + \dots \\ \frac{1}{\overline{DP}_n} &= \frac{1}{\overline{DP}_{n,0}} + C_S \frac{[S]}{[M]} + C_T \frac{[T]}{[M]} + \dots \end{aligned}$$



See Odian P.235

chain transfer coefficient C_S

10.6 Temperature Dependence of R_p and $\overline{DP}_n$

Assume : no chain transfer

$$R_p = k_p \left\{ \left(\frac{k_d}{k_t} \right) f \cdot [I_2] \right\}^{\frac{1}{2}} [M]$$

$$\ln R_p = \ln [M] + \ln \left[k_p \left(\frac{k_d}{k_t} \right)^{\frac{1}{2}} \right] + \ln [f [I_2]]^{\frac{1}{2}} \dots \dots (1)$$

$$k_p = k_p^\circ e^{-E_p / RT} \quad E_p \quad 5 \sim 8 \text{ kcal / mole}$$

$$k_d = k_d^\circ e^{-E_d / RT} \quad E_d \quad 30 \text{ kcal / mole}$$

$$k_t = k_t^\circ e^{-E_t / RT} \quad E_t \quad 2 \sim 5 \text{ kcal / mole}$$

From Eq(1), and assume $[I_2], [M] = \text{const}$, f independent of T .

$$\begin{aligned} \frac{d \ln R_p}{dT} &= \frac{d \ln \left[k_p \left(\frac{k_d}{k_t} \right)^{\frac{1}{2}} \right]}{dT} \\ &= \frac{E_p - \frac{E_t}{2} + \frac{E_d}{2}}{RT^2} = \frac{7 - 2 + 15}{RT^2} > 0 \end{aligned}$$

$\therefore$ slope of $\ln R_p / T$ is positive (+)

$\therefore$ as $T \uparrow$ $\ln R_p \uparrow$

but rate of increase $\downarrow$ as $d \ln R_p / dT \downarrow$

$$\overline{DP}_n = \frac{2 R_p}{R_t(1 + y)} \quad , \quad n = \frac{R_p}{R_t} = \frac{R_p}{R_i}$$

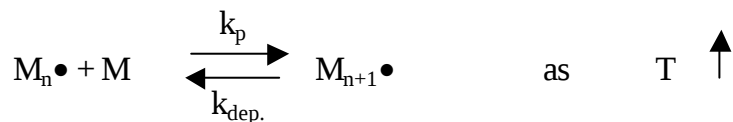
$$\frac{d \ln n}{dT} = \frac{E_p - \frac{E_t}{2} - \frac{E_d}{2}}{RT^2} = \frac{7 - 2 - 15}{RT^2} < 0$$

$\therefore$ as $T \uparrow$, $\ln n \downarrow$ $\overline{DP}_n \downarrow$

$[I] \uparrow \quad R_p \uparrow \quad \text{but} \quad \overline{DP}_n \downarrow$
 $T \uparrow \quad n \downarrow \quad \overline{DP}_n \downarrow$

10.7 Ceiling Temperature-Polymerization-Depolymerization

Equilibria.



$$\text{Equilibrium const} \quad K = \frac{[M_{n+1} \bullet]}{[M_n \bullet][M]} = \frac{1}{[M]}$$

$$\Delta G = \Delta H - T \Delta S$$

$$= \Delta G^\circ + RT \ln K \quad \text{for any chemical rxn.}$$

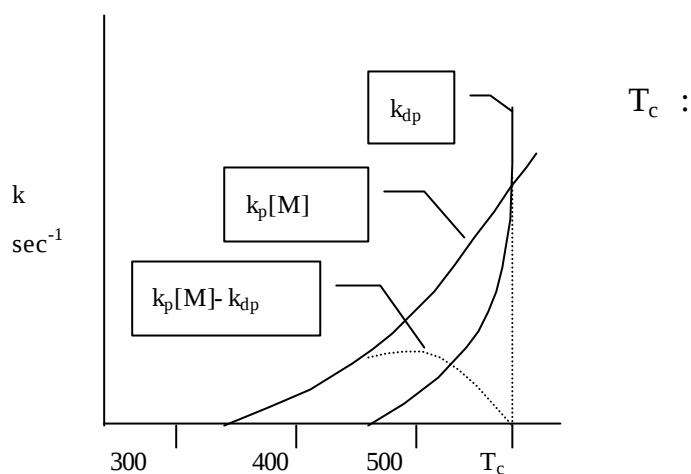
$$\text{at eq. } \Delta G = 0$$

$$\therefore \ln K = -\frac{\Delta G^\circ}{RT} = -\frac{\Delta H^\circ - T \Delta S^\circ}{RT} = -\frac{\Delta H^\circ}{RT} + \frac{\Delta S^\circ}{R}$$

$$\Delta G^\circ = \Delta H^\circ - T \Delta S^\circ$$

$$T_c = \frac{\Delta H^\circ}{\Delta S^\circ + R \ln [M]_c} \quad \text{Ceiling Temperature}$$

∴ for each $[M]_c$ get various T_c



Odian Fig 3-18

Monomer	$-\Delta H^\circ$ kcal/g mole	T_c °C (bulk)
Styrene	16	235
MMA	13	164
Ethylene	26	407
Propylene	21	300
α -methyl Styrene	7	6

Entropy changes for all polymers are not so different.

$$\Delta S_p = S_p - S_m \quad S_p \text{ 가 } \text{negative}(-) \text{ value } \text{가}$$

$$\Delta H_p = H_p - H_m \quad - \text{ exothermic.}$$

10.8 Trommsdorff Effect or Gel Effect.

Remember $-\frac{d[I]}{dt} = k_d [I] \quad [I] = [I_0] e^{-k_d t}$

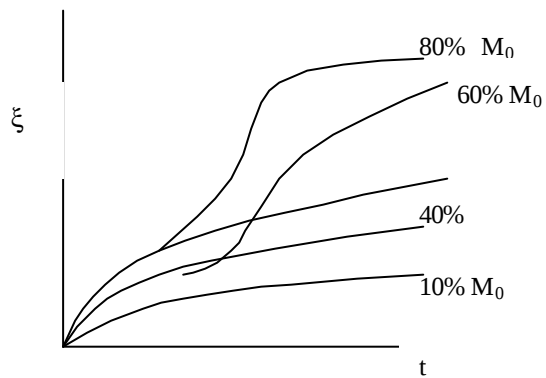
k_d 가 $[I] \approx [I_0]$

At CSTR, conc. is const, Batch reactor, conc. const.

$$v_p = -\frac{d[M]}{dt} \approx \text{const } [M] \quad \frac{[M]}{[M_0]} = e^{-kt}$$

$$\% \text{ conversion} = \frac{[M_0] - [M]}{[M_0]} = 1 - \frac{[M]}{[M_0]} = x$$

$$x = 1 - e^{-kt} \therefore \text{one would expect } \hat{t} \downarrow \text{ as } t \uparrow \quad \hat{t} \uparrow \text{ as } [M_0] \uparrow$$



autoacceleration
as $[M_0] \uparrow$ drastic $\uparrow \xi$.